

# MAGNETOHYDRODYNAMIC FLOW PAST A POROUS ROTATING DISK IN A CIRCULAR MAGNETIC FIELD

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## SUMMARY

This paper studies the effects of a circular magnetic field on the flow of a conducting fluid about a porous rotating disk. Using modern quasi-Newton and globally convergent homotopy methods, numerical solutions are obtained for a wide range of magnetic field strengths, suction and injection velocities and Alfvén and disk speeds. Results are presented graphically in terms of three non-dimensional parameters. There is excellent agreement with previous work and asymptotic formulae.

KEY WORDS Magnetohydrodynamics Homotopy Quasi-Newton Rotating disk

## INTRODUCTION

The flow past a rotating disk in a viscous fluid has received considerable attention in the past few decades. Von Karman<sup>1</sup> first obtained a solution for this problem. Later Cochran<sup>2</sup> obtained a more accurate solution by numerical integration of the governing equations. The effects of suction and injection at the disk surface were studied later by Stuart,<sup>3</sup> Sparrow and Gregg,<sup>4</sup> Kuiken<sup>5</sup> and Ackroyd.<sup>6</sup>

The rotating disk problem in the presence of an axial magnetic field was studied by Sparrow and Cess,<sup>7</sup> Rizvi<sup>8</sup> (whose mathematical formulation and numerical solutions are incorrect) and Pande.<sup>9</sup> Pao<sup>10</sup> studied the flow of a viscous electrically conducting fluid past a rotating disk with a circular magnetic field at the disk surface.

In the present investigation we study the effects of surface suction and injection on the flow past a rotating disk in the presence of a circular magnetic field. The governing equations are similar to those derived by Pao.<sup>10</sup> Here we assume that there is no magnetic field in the fluid far from the disk and also that there is a field in the tangential direction in the boundary layer generated by external means within the disk itself. Such a field has application in the shielding of a rotating body from excessive heating.<sup>10</sup>

The governing partial differential equations of the problem are reduced to non-linear ordinary differential equations using similarity transformations. The system is then solved numerically

using quasi-Newton and homotopy methods. The flow depends on the non-dimensional parameters  $\alpha$  (magnetic Prandtl number),  $\beta$  (ratio of Alfvén speed to disk speed) and  $A$  (suction or injection parameter).

### FORMULATION OF THE PROBLEM

The governing equations in cylindrical polar co-ordinates  $(r, \theta, z)$  for an incompressible, viscous, electrically conducting fluid in axisymmetric steady motion<sup>8</sup> are

$$u \frac{\partial u}{\partial r} + w \frac{\partial u}{\partial z} - \frac{v^2}{r} + \frac{\partial P}{\partial r} - f \frac{\partial f}{\partial r} - h \frac{\partial f}{\partial z} + \frac{g^2}{r} - v \left( \nabla^2 u - \frac{u}{r^2} \right) = 0, \quad (1)$$

$$u \left( \frac{\partial v}{\partial r} + \frac{v}{r} \right) + w \frac{\partial v}{\partial z} - f \left( \frac{\partial g}{\partial r} + \frac{g}{r} \right) - h \frac{\partial g}{\partial z} - v \left( \nabla^2 v - \frac{v}{r^2} \right) = 0, \quad (2)$$

$$u \frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} + \frac{\partial P}{\partial z} - f \frac{\partial h}{\partial r} - h \frac{\partial h}{\partial z} - v \nabla^2 w = 0, \quad (3)$$

$$\frac{\partial}{\partial r}(ru) + \frac{\partial}{\partial z}(rw) = 0, \quad (4)$$

$$\frac{\partial}{\partial r}(rf) + \frac{\partial}{\partial z}(rh) = 0, \quad (5)$$

$$\frac{\partial}{\partial r}(vf - ug) + \frac{\partial}{\partial z}(vh - wg) + \eta \left( \nabla^2 g - \frac{g}{r^2} \right) = 0, \quad (6)$$

$$(uh - wf) - \eta \left( \frac{\partial h}{\partial r} - \frac{\partial f}{\partial z} \right) = 0, \quad (7)$$

where

$$\nabla^2 = \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{\partial^2}{\partial z^2}$$

and  $u, v, w$  and  $f, g, h$  are the components of velocity and normalized magnetic field strength respectively in the  $r, \theta, z$  directions respectively.  $\nu$  is the kinematic viscosity,  $\eta = 1/\mu\sigma$  is the magnetic diffusivity,  $\mu$  is the magnetic permeability and  $\sigma$  is the electrical conductivity. Here

$$(f, g, h) = (f_1, g_1, h_1)(\mu/\rho)^{1/2} \quad \text{and} \quad P = (f^2 + g^2 + h^2)/2 + p/\rho + \chi,$$

where  $f_1, g_1, h_1$  are the components of the magnetic field,  $p$  is the fluid pressure,  $\rho$  is the uniform density and  $\chi$  is the potential for a unit mass of the conservative body forces. It is assumed that  $\nu, \sigma$  and  $\mu$  are constants and the net charge density is zero.

### SIMILARITY SOLUTION AND BOUNDARY CONDITIONS

The disk surface is in the plane  $z=0$  and rotates about the  $z$ -axis with constant angular velocity  $\omega$ . An axial electric current of uniform current density  $J_0$  is imposed at the disk surface. Equivalently, a tangential magnetic field component  $g = \Omega r$  is imposed at the disk surface, with  $\Omega = (\mu/\rho)^{1/2}(J_0/2)$  a constant, and  $f$  and  $h$  are zero.

Using the similarity transformations

$$\begin{aligned} u &= \omega r m'(\zeta), & w &= -2(\nu\omega)^{1/2} m(\zeta), & P &= \nu\omega S(\zeta), \\ v &= \omega r G(\zeta), & g &= \Omega r M(\zeta), & \zeta &= z(\omega/\nu)^{1/2}, \end{aligned} \quad (8)$$

equations (1)–(7) reduce to

$$m''' + 2mm'' - (m')^2 + G^2 - \beta^2 M^2 = 0, \quad (9)$$

$$2(mG' - m'G) + G'' = 0, \quad (10)$$

$$M'' + 2\alpha m M' = 0, \quad (11)$$

$$S' + 4mm' + 2m'' = 0, \quad (12)$$

where  $\alpha = \nu/\eta$  is the magnetic Prandtl number and  $\beta = \Omega/\omega$  is the ratio of the Alfvén speed to the disk speed. Note that equation (12) decouples from the others and  $S(\zeta)$  is easily obtained once  $m(\zeta)$  is known.

It is assumed that the disk is porous and that either suction or injection occurs at the disk surface such that

$$w(0) = -2\sqrt{(\nu\omega)}A,$$

so  $A > 0$  corresponds to suction and  $A < 0$  corresponds to injection. The other boundary conditions are

$$\begin{aligned} u(0) &= 0, & v(0) &= \omega r, \\ u(\infty) &= 0, & v(\infty) &= 0. \end{aligned}$$

The boundary conditions for equations (9)–(12) are

$$m(0) = A, \quad m'(0) = 0, \quad G(0) = 1, \quad M(0) = 1, \quad (13)$$

$$m'(\zeta) \rightarrow 0, \quad G(\zeta) \rightarrow 0, \quad M(\zeta) \rightarrow 0, \quad S(\zeta) \rightarrow 0 \quad \text{as } \zeta \rightarrow \infty. \quad (14)$$

## NUMERICAL METHOD

The computation of  $S(\zeta)$  is straightforward and is not discussed here. Following the format in Heruska,<sup>11</sup> define

$$\mathbf{X} = \begin{pmatrix} m''(0) \\ G'(0) \\ M'(0) \end{pmatrix}. \quad (15)$$

Let  $m(\zeta; \mathbf{X})$ ,  $G(\zeta; \mathbf{X})$ ,  $M(\zeta; \mathbf{X})$  be the solution of the initial value problem given by equations (9)–(11) with initial conditions (13) and (15). The original two-point boundary value problem given by equations (9)–(11) and (13) is numerically equivalent to solving the non-linear system of equations

$$\mathbf{F}(\mathbf{X}) = \begin{pmatrix} m'(\tau; \mathbf{X}) \\ G(\tau; \mathbf{X}) \\ M(\tau; \mathbf{X}) \end{pmatrix} = 0, \quad (16)$$

where  $\tau$  is chosen large enough such that

$$|m'(\zeta) - m'(\tau)| + |G(\zeta) - G(\tau)| + |M(\zeta) - M(\tau)| < \varepsilon$$

for  $\tau < \zeta < \infty$  and a given  $\varepsilon > 0$ . Equation (16) is derived from the boundary conditions (14). Algorithms for solving non-linear systems like (16) typically require partial derivatives such as  $\partial m'/\partial X_k$ . We can write the functions needed as

$$\mathbf{Y} = \left( m, m', m'', G, G', M, M', \frac{\partial m}{\partial X_k}, \frac{\partial m'}{\partial X_k}, \frac{\partial m''}{\partial X_k}, \frac{\partial G}{\partial X_k}, \frac{\partial G'}{\partial X_k}, \frac{\partial M}{\partial X_k}, \frac{\partial M'}{\partial X_k} \right)$$

for  $k = 1, 2, 3$ , where  $m$ ,  $G$  and  $M$  are functions of  $\zeta$ . Now  $m'(\zeta)$ ,  $G(\zeta)$ ,  $M(\zeta)$  and their partial derivatives can be calculated from the first-order system

$$\begin{aligned}
 Y'_1 &= Y_2, \\
 Y'_2 &= Y_3, \\
 Y'_3 &= \beta^2 Y_6^2 + Y_2^2 - Y_4^2 - 2Y_1 Y_3, \\
 Y'_4 &= Y_5, \\
 Y'_5 &= -2(Y_1 Y_5 - Y_2 Y_4), \\
 Y'_6 &= Y_7, \\
 Y'_7 &= -2\alpha Y_1 Y_7, \\
 Y'_8 &= Y_9, \\
 Y'_9 &= Y_{10}, \\
 Y'_{10} &= 2(\beta^2 Y_6 Y_{13} - Y_4 Y_{11} - Y_3 Y_8 - Y_1 Y_{10} + Y_2 Y_9), \\
 Y'_{11} &= Y_{12}, \\
 Y'_{12} &= 2(Y_9 Y_4 + Y_2 Y_{11} - Y_1 Y_{12} - Y_8 Y_5), \\
 Y'_{13} &= Y_{14}, \\
 Y'_{14} &= -2\alpha(Y_8 Y_7 + Y_1 Y_{14}), \\
 \mathbf{Y}(0) &= (A, 0, X_1, 1, X_2, 1, X_3, 0, 0, \delta_{1k}, 0, \delta_{2k}, 0, \delta_{3k}),
 \end{aligned}$$

where  $\delta_{ik}$  is the Kronecker delta. By solving this system three times, for  $k = 1, 2, 3$ , the Jacobian matrix  $\mathbf{DF}(\mathbf{X})$  of  $\mathbf{F}(\mathbf{X})$  can be calculated.

Two methods were utilized to solve this problem, a quasi-Newton least-change secant update method and a globally convergent homotopy method. The quasi-Newton code used was HYBRJ from the MINPACK subroutine package from Argonne National Laboratory.<sup>12</sup> These quasi-Newton routines are robust and usually quite efficient. However, they fail at times by converging to local minima of  $\mathbf{F}(\mathbf{X})^T \mathbf{F}(\mathbf{X})$  which are not solutions of  $\mathbf{F}(\mathbf{X}) = 0$ .

The other method, a globally convergent homotopy method from the subroutine package HOMPAC developed by Watson *et al.*,<sup>13</sup> does not suffer from the convergence problems of the quasi-Newton method. However, this method requires considerably more computation time. Details about the homotopy algorithm and some of its applications can be found in References 14–17.

The computational strategy here was to try to solve (16) first using the relatively inexpensive quasi-Newton method. If that failed, then the expensive, but guaranteed convergent, homotopy algorithm was used.

As previously mentioned, these quasi-Newton and homotopy methods use some partial derivatives with respect to the initial conditions. For some values of  $A$ ,  $\alpha$  and  $\beta$ , these partials increase drastically as  $\tau$  increases. This results in numerical instability in cases where  $A < -1$  (i.e. large injection) and  $\alpha > 10$ . Also, cases of large injection and large  $\beta$  cause  $M(\zeta)$  to approach zero very slowly. This requires  $\tau$  to be very large, which also causes numerical instability. Such instabilities are inherent with shooting, on which the definition of  $\mathbf{F}(\mathbf{X})$  is based. Other ways of discretizing the two-point boundary value problem (9)–(14), such as finite differences, collocation and finite elements, will be considered in future work.

DISCUSSION

Figure 1 shows the effect of  $A$  on  $m'$ ,  $G$ ,  $m$  and  $M$  for  $\alpha=0.5$  and  $\beta=0.2$ . The case  $A=0$  corresponds to the impermeable disk<sup>10</sup> in all the figures. The effect of  $A$  on axial velocity is shown in Figure 1(a). As suction ( $A > 0$ ) increases, the axial velocity becomes almost constant and maintains the suction value throughout the boundary layer. When fluid is injected at the disk surface ( $A < 0$ ), the incoming axial flow is retarded by the injected fluid. The greater the injection velocity, the more the inflow is opposed. This results in decreasing the axial velocity at infinity and moving the crossover point away from the disk. The radial velocity  $m'$  is shown in Figure 1(b). The radial velocity increases monotonically from zero at the disk surface to a maximum near the disk and then decreases monotonically to zero at the edge of the boundary layer. As the injection velocity increases, the maximum for the radial velocity increases and moves away from the disk. Increased suction velocity decreases the maximum and moves it closer to the disk. The radial velocity becomes almost zero for large suction values causing the flow to be two-dimensional. Figure 1(c) shows the variation in tangential velocity  $G$  due to changes in  $A$ . The boundary layer thickness decreases with increased suction and increases with increased injection velocity. The thickness of the boundary layer for the magnetic field  $M$  also increases with injection and decreases with suction (Figure 1(d)).

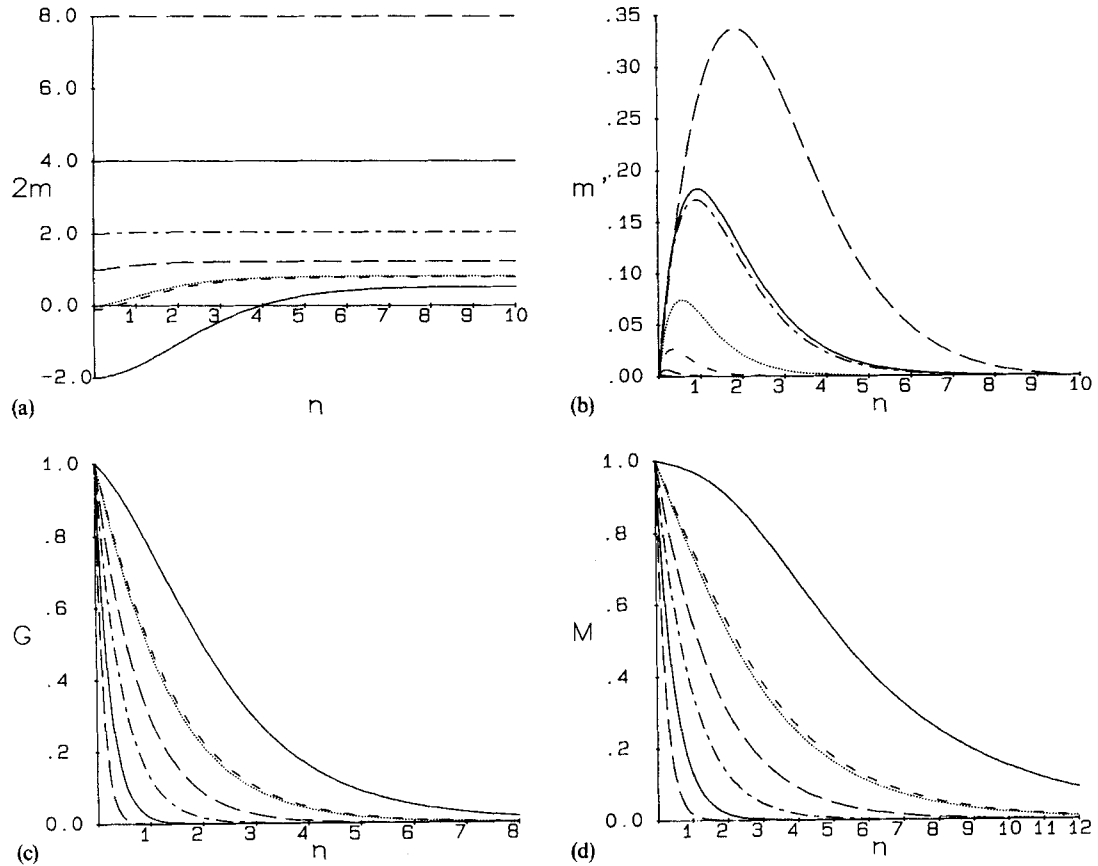


Figure 1. Effect of  $A$  on flow and magnetic field with  $\alpha=0.5$  and  $\beta=0.2$ : (a) axial velocity,  $A=4, 2, 1, 0.5, 0, -0.01, -1$  (top to bottom); (b) radial velocity,  $A=-1, -0.05, 0, 0.5, 1, 2, 4$  (top to bottom); (c) tangential velocity,  $A=-1, -0.05, 0, 0.5, 1, 2, 4$  (top to bottom); (d) magnetic field,  $A=-1, -0.05, 0, 0.5, 1, 2, 4$  (top to bottom)

Computations indicate that the effect of  $\alpha$  on  $m, m'$  and  $G$  is small and consequently plots of  $m, m'$  and  $G$  for varying  $\alpha$  are not included. Increasing  $\alpha$  causes only a small increase in  $m$  near the disk. A slightly larger increase occurs at infinity. However, this increase diminishes as  $\alpha$  gets large; there is almost no change in  $m$  between  $\alpha=5$  and  $\alpha=10$ . Similarly, an increase in  $\alpha$  causes a small and diminishing increase in the radial velocity. The tangential velocity is slightly decreased by an increase in  $\alpha$ . The effect of  $\alpha$  on the magnetic field  $M$  is shown in Figure 2(a). For large values of  $\alpha$ , the magnetic field maintains the same strength as at the disk surface for a small distance from the disk and then falls to its edge strength in a very short distance. A higher value of injection ( $A = -1$ ) gives similar effects of  $\alpha$  on  $m, m'$  and  $G$  (not shown), but has a more pronounced effect on  $M$  (Figure 2(b)). The parameter  $\alpha$  has the same effect on  $m, m'$  and  $G$  when there is suction ( $A = 0.5$ ) as when there is injection. The only relevant difference is that  $m'$  peaks at a much lower level. Increasing  $\alpha$  in the presence of suction causes  $M$  to fall to the edge strength quickly (Figure 2(c)).

Figure 3 shows the effect of  $\beta$  on the flow fields when suction ( $A = 1$ ) is applied and  $\alpha = 1$ . As  $\beta$  gets large, the axial flow (Figure 3(a)) towards the disk decreases and becomes a constant throughout the boundary layer when  $\beta = 1$ . When  $\beta$  increases, the radial velocity (Figure 3(b)) decreases and disappears at  $\beta = 1$ . The effect of  $\beta$  on the tangential velocity and the magnetic field is not very pronounced, so is not shown.

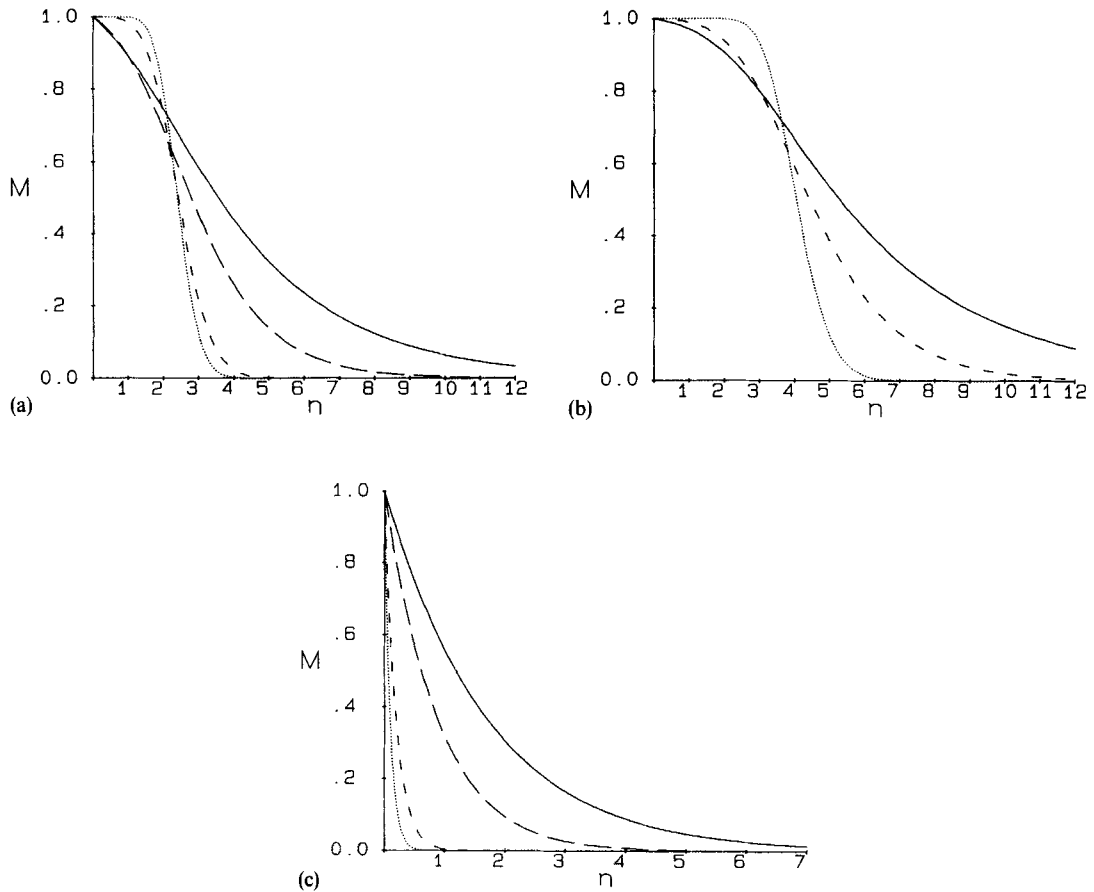


Figure 2. Effect of  $\alpha$  on magnetic field with  $\beta=0.2$ : (a)  $A = -0.5, \alpha = 10, 5, 1, 0.5$  (dotted, short dashed, long dashed, solid); (b)  $A = -1, \alpha = 5, 1, 0.5$  (dotted, dashed, solid); (c)  $A = 0.5, \alpha = 10, 5, 1, 0.5$  (dotted, short dashed, long dashed, solid)

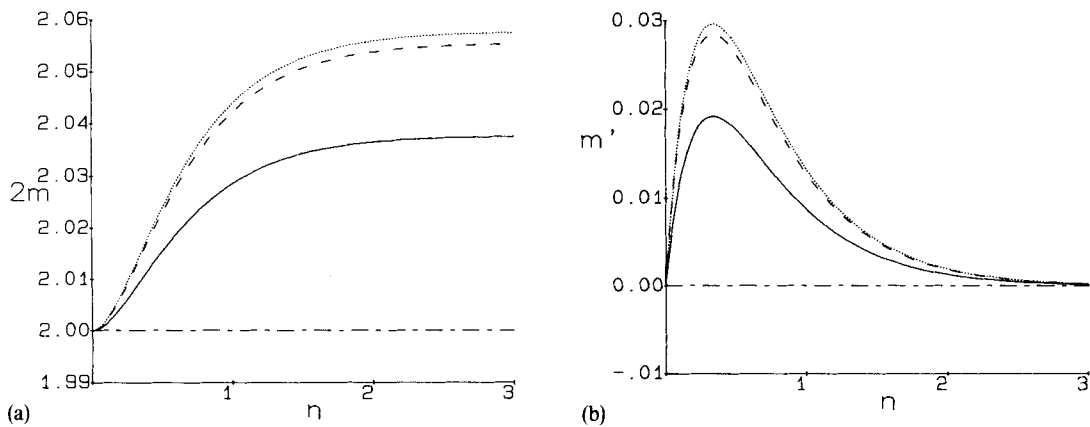


Figure 3. Effect of  $\beta$  on flow fields with  $A = 1$ ,  $\alpha = 1$  and  $\beta = 0, 0.2, 0.6, 1$  (dotted, dashed, solid, dash-dot): (a) axial velocity; (b) radial velocity

Table I. Effect of  $A$ ,  $\alpha$ , and  $\beta$  on  $m(\infty)$ ,  $m''(0)$ ,  $M'(0)$  and  $G'(0)$

$A$	$\alpha$	$\beta$	$2m(\infty)$	$m''(0)$	$-M'(0)$	$-G'(0)$
4.00	0.5	0.2	8.0008	0.05749	4.00023	8.00057
2.00	0.5	0.2	4.0066	0.11479	2.00180	4.00456
1.00	0.5	0.2	2.0490	0.22387	1.01351	2.03422
0.50	0.5	0.2	1.2301	0.36553	0.56466	1.16202
0.00	0.5	0.2	0.8223	0.48806	0.25234	0.60054
-0.05	0.5	0.2	0.7999	0.49210	0.22968	0.56088
-1.00	0.5	0.2	0.5111	0.38300	0.01678	0.13083
-0.50	0.5	0.2	0.6560	0.46997	0.08367	0.29220
-0.50	1.0	0.2	0.7249	0.46982	0.06460	0.29280
-0.50	5.0	0.2	0.7395	0.46826	0.00072	0.29178
-0.50	10.0	0.2	0.7392	0.46799	0.00000	0.29138
-1.00	0.5	0.2	0.5111	0.38300	0.01678	0.13083
-1.00	1.0	0.2	0.6441	0.38278	0.00334	0.13070
-1.00	5.0	0.2	0.6642	0.38267	0.00000	0.13055
0.50	0.5	0.2	1.2301	0.36553	0.56466	1.16202
0.50	1.0	0.2	1.2530	0.37531	1.08979	1.17023
0.50	5.0	0.2	1.2602	0.38587	5.07951	1.17484
0.50	10.0	0.2	1.2605	0.38764	10.05441	1.17511
-0.50	1.0	0.0	0.7607	0.48948	0.06982	0.30217
-0.50	1.0	0.1	0.7524	0.48459	0.06855	0.29988
-0.50	1.0	0.2	0.7249	0.46982	0.06461	0.29280
-0.50	1.0	0.3	0.6680	0.44495	0.05391	0.28026
-0.50	1.0	0.4	0.5212	0.40954	0.04441	0.26031
1.00	1.0	0.0	2.0578	0.24242	2.01941	2.03853
1.00	1.0	0.2	2.0556	0.23290	2.01867	2.03707
1.00	1.0	0.6	2.0378	0.15625	2.01266	2.02519
1.00	1.0	1.0	2.0000	0.00000	2.00000	2.00000

The effect of  $\beta$  on the flow fields when fluid is injected at the disk surface (negative  $A$ ) and  $\alpha = 1$  is slight and is not shown. The axial velocity decreases as  $\beta$  increases. The effect is more pronounced at infinity but still small. As  $\beta$  gets large, an increase in  $\beta$  causes larger decreases in  $m$  at infinity. As  $\beta$  increases, the crossover point from negative to positive flow moves away from the disk. An increase in  $\beta$  decreases the radial velocity. Again, this change increases as  $\beta$  increases. However, the tangential velocity and the magnetic field strength increase as  $\beta$  increases.

From Table I we can see that changes in  $A$  have a more pronounced effect on  $G'(0)$  than do changes in  $\alpha$  and  $\beta$ . Changes in  $\alpha$  have a very small effect on  $G'(0)$ . As  $A$  gets smaller (which decreases  $|G'(0)|$ ), the effect of  $A$  decreases. However, as  $\beta$  gets larger (which also decreases  $|G'(0)|$ ) there is an increasing effect on  $G'(0)$ .

From Table I, critical values (where  $G'(0) = 0$ ) of  $A$ ,  $\alpha$  and  $\beta$  would occur for small  $A$  and large  $\beta$ . It is apparent from the  $M'(0)$  column that  $M'(0)$  approaches zero faster than  $G'(0)$  does. Thus shooting needs to use a large  $\tau$  for  $G$  and  $M$  to converge to zero. As previously mentioned, this results in numerical instability, and considerable computational difficulty was encountered attempting to find critical values. To find values for  $A$ ,  $\alpha$  and  $\beta$  where  $G'(0) = 0$ , an expensive and involved multiple-shooting technique<sup>18</sup> was employed. Using this technique, values for  $G'(0)$  close to zero were obtained by varying  $\beta$  and keeping  $A = 0.1$  and  $\alpha = 1.0$ . Using three data points close to zero, quadratic extrapolation to the limit yielded  $\beta = 1.1072$ .

Table II shows excellent agreement of our results with the approximate analytic solution obtained by Pao<sup>10</sup> for  $A = 0$ . The maximum percentage difference in Table II is 0.197% for  $m'(0)$ , 0.174% for  $G'(0)$ , 0.391% for  $M'(0)$  and 2.016% for  $2m(\infty)$ , the latter occurring at  $\alpha = 1.0$ ,  $\beta = 0.70$ .

Table II. Comparison of current results with those of Pao<sup>10</sup> (hatted)

$\alpha$	$\beta$	$\hat{m}'(0)$	$m'(0)$	$-\hat{G}'(0)$	$-G'(0)$	$-\hat{M}'(0)$	$-M'(0)$	$2\hat{m}(\infty)$	$2m(\infty)$
0.5	0.00	0.51024	0.51023	0.61592	0.61592	0.26227	0.26229	0.884	0.884
0.5	0.05	0.50886	0.50885	0.61501	0.61501	0.26170	0.26172	0.882	0.881
0.5	0.10	0.50470	0.50471	0.61223	0.61223	0.25997	0.25997	0.871	0.870
0.5	0.15	0.49778	0.49779	0.60749	0.60748	0.25696	0.25692	0.852	0.852
0.5	0.20	0.48806	0.48806	0.60054	0.60054	0.25236	0.25234	0.823	0.822
0.5	0.25	0.47550	0.47550	0.59102	0.59100	0.24573	0.24566	0.778	0.777
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1.0	0.00	0.51024	0.51023	0.61592	0.61592	0.39625	0.39625	0.884	0.884
1.0	0.10	0.50558	0.50558	0.61363	0.61363	0.39469	0.39469	0.880	0.880
1.0	0.20	0.49154	0.49154	0.60657	0.60657	0.38991	0.38991	0.867	0.867
1.0	0.30	0.46786	0.46786	0.59423	0.59423	0.38152	0.38152	0.844	0.844
1.0	0.40	0.43406	0.43405	0.57552	0.57552	0.36872	0.36874	0.809	0.809
1.0	0.50	0.38936	0.38936	0.54836	0.54834	0.34998	0.34998	0.755	0.755
1.0	0.60	0.33266	0.33265	0.50822	0.50816	0.32186	0.32175	0.669	0.669
1.0	0.70	0.26296	0.26289	0.44319	0.44242	0.27451	0.27344	0.506	0.496
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10.0	0.00	0.51024	0.51023	0.61592	0.61592	1.13399	1.13412	0.884	0.884
10.0	0.20	0.50058	0.50057	0.61378	0.61378	1.12916	1.12915	0.883	0.883
10.0	0.40	0.47120	0.47119	0.60717	0.60717	1.11380	1.11379	0.878	0.878
10.0	0.60	0.42078	0.42078	0.59540	0.59540	1.08638	1.08638	0.870	0.870
10.0	0.80	0.34650	0.34650	0.57695	0.57695	1.04322	1.04322	0.857	0.857
10.0	1.00	0.24202	0.24201	0.54816	0.54816	0.97545	0.97545	0.838	0.838
10.0	1.20	0.08714	0.08713	0.49600	0.49600	0.85155	0.85155	0.805	0.805
10.0	1.30	-0.07124	-0.07110	0.41399	0.41412	0.65578	0.65606	0.757	0.759



Table III. Comparison of obtained values with asymptotic formula values (hatted)

$A$	$\alpha$	$\beta$	$m'(0)$	$\hat{m}'(0)$	% diff.	$-G'(0)$	$-\hat{G}'(0)$	% diff.	$-M'(0)$	$-\hat{M}'(0)$	% diff.
4.0	0.5	0.2	0.05749	0.0575	0.017	8.00057	8	0.007	4.00023	4.0	0.006
2.0	0.5	0.2	0.11479	0.1150	0.183	4.00456	4	0.114	2.00180	2.0	0.090
1.0	0.5	0.2	0.22387	0.2300	2.738	2.03422	2	1.682	1.01351	1.0	1.333
0.5	0.5	0.2	0.36553	0.4600	25.845	1.62020	1	13.652	0.56466	0.5	11.451
2.0	0.5	0.2	0.11479	0.1150	0.183	4.00456	4	0.114	2.00180	2.0	0.090
2.0	1.0	0.2	0.11975	0.1200	0.209	4.00497	4	0.124	4.00249	4.0	0.062
2.0	5.0	0.2	0.12374	0.1240	0.210	4.00517	4	0.129	20.00185	20.0	0.009
2.0	10.0	0.2	0.12424	0.1245	0.211	4.00518	4	0.129	40.00118	40.0	0.003
2.0	0.5	0.2	0.11479	0.1150	0.183	4.00456	4	0.114	2.00180	2.0	0.090
2.0	0.5	0.4	0.08491	0.0850	0.104	4.00270	4	0.067	2.00097	2.0	0.048
2.0	0.5	0.6	0.03499	0.0350	0.033	3.99958	4	0.011	1.99958	2.0	0.021
2.0	0.5	0.8	-0.03517	-0.0350	0.487	3.99517	4	0.121	1.99762	2.0	0.119
2.0	0.5	1.0	-0.12585	-0.1250	0.672	3.98944	4	0.265	1.99507	2.0	0.247

## ASYMPTOTIC COMPARISONS

Applying standard perturbation techniques to equations (9)–(11) for large  $A$  and small  $\alpha$  and  $\beta$ , we get

$$G'(0) \approx \hat{G}'(0) = -2A,$$

$$M'(0) \approx \hat{M}'(0) = -2A\alpha,$$

$$m''(0) \approx \hat{m}''(0) = \frac{\alpha - \beta^2}{4A\alpha}.$$

From Table III we see that the asymptotic formula values compare favourably with the results obtained for  $A \geq 1$ . Also, changes in  $\alpha$  do not affect the goodness of the asymptotic formulae within the range studied. Furthermore, there is good agreement for  $\beta$  values less than 1.0.

## CONCLUSIONS

The rotating disk acts as a centrifugal fan. The radial flow is balanced by an induced axial flow towards the rotating disk. When suction is applied at the disk surface, the radial flow decreases, the axial flow at infinity increases towards the disk and the boundary layer thickness decreases. The opposite effect is observed when the fluid is injected at the disk surface; the radial velocity increases, the axial velocity at infinity decreases and the boundary layer thickens. With an impermeable rotating disk, an increase in  $\beta$  decreases the axial velocity at infinity and increases the boundary layer thickness. As  $\alpha$  increases, the boundary layer thicknesses of the flow and magnetic field decrease.

The effect of the magnetic Prandtl number  $\alpha$  on the fluid flow is negligible. Similarly, the effect of  $\beta$  on the magnetic field is negligible. Conversely, the effects of  $\alpha$  on the magnetic field and  $\beta$  on the fluid flow are more significant.

The tables and figures here show the effect of the parameters  $A$ ,  $\alpha$  and  $\beta$  on the fluid flow and magnetic field for order-of-magnitude variations in the parameters. These data would apply to applications in magnetohydrodynamic heat shielding, for example.

## ACKNOWLEDGEMENTS

S. K. Kumar was supported by a fellowship from CSIR, India. L. T. Watson was supported in part by Air Force Office of Scientific Research Grant 85-0250.

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